

Introduction of Kimura Laboratory



Research topics



Development of Mid-Story Pin Connection System
Preventing Column Yield and Assessment of Ultimate
Seismic Capacity of Steel Moment Resisting Frames

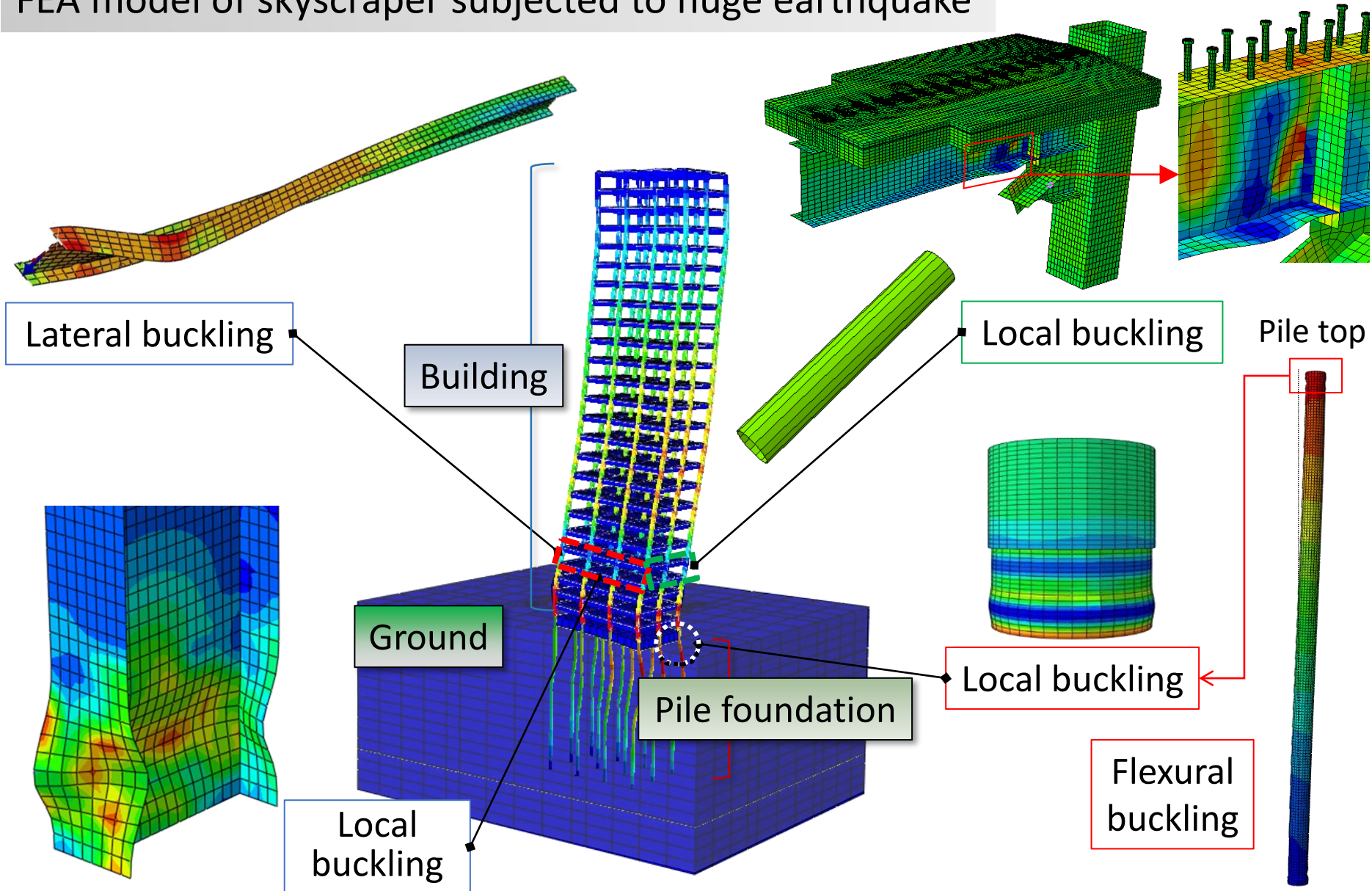
Construction of Ultimate State Design Method of Steel
Piles and Elucidation of Dynamic Buckling Behavior of
Steel Piles in Liquefied Soil

Invention of Evaluation Method of Lateral
Buckling Strength of Large-Span Beams

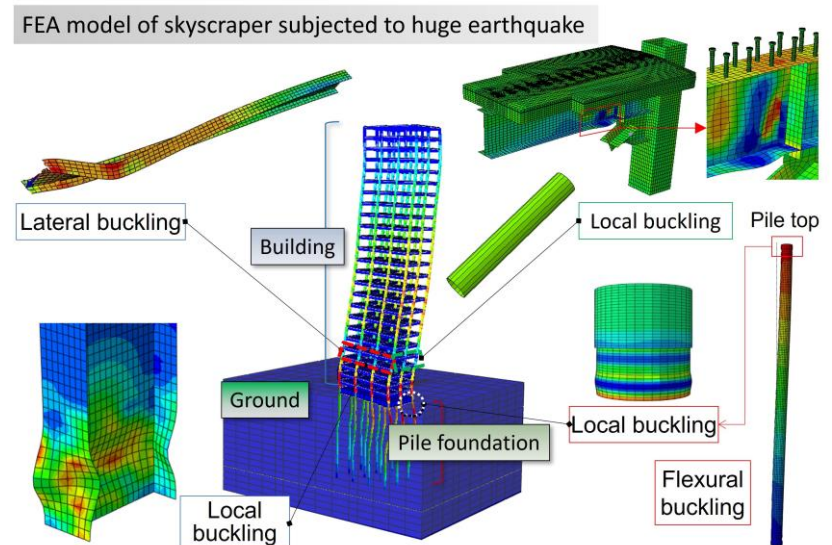
Creation of Seismic Design Method of Buckling
Restrained Braced Frame with Concrete Slab

Research topics

FEA model of skyscraper subjected to huge earthquake

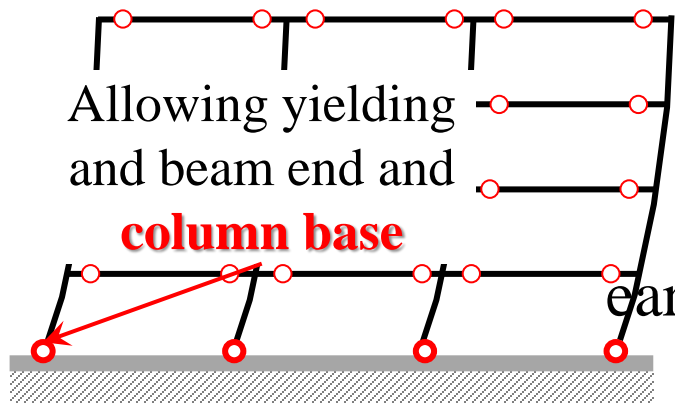


Development of Mid-Story Pin Connection System Preventing Column Yield and Assessment of Ultimate Seismic Capacity of Steel Moment Resisting Frames

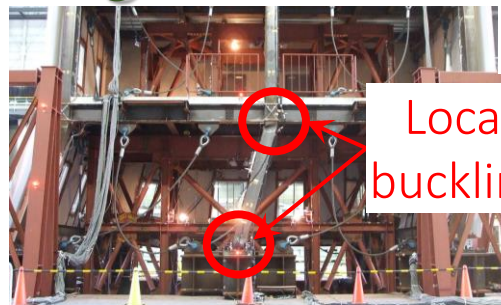


Development of new column base system

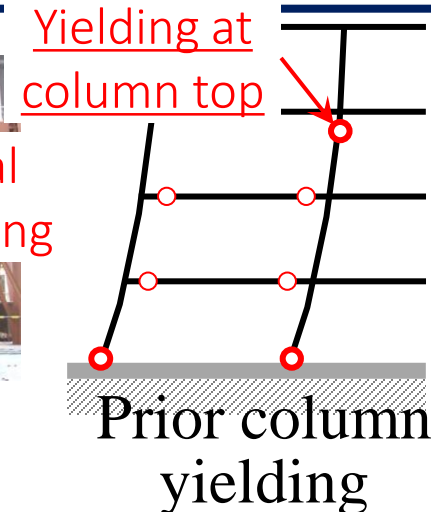
Conventional moment resisting frame



Huge earthquake



Story collapse at 1st story

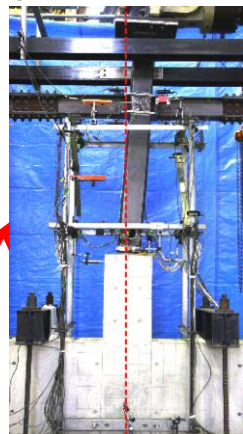
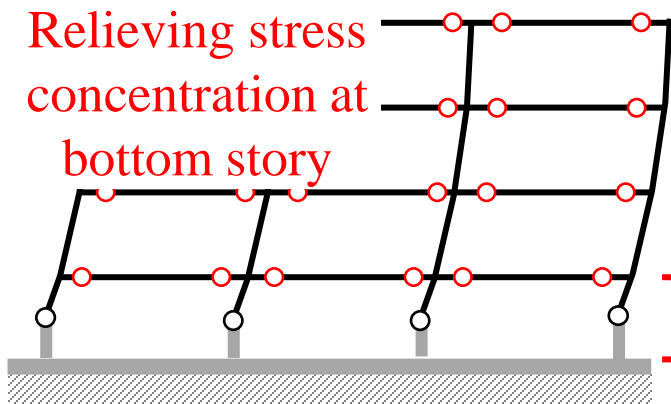


Relieving stress at hot-spot of structure

New steel moment resisting frame

1) Mid-story pin-support system

Relieving stress concentration at bottom story



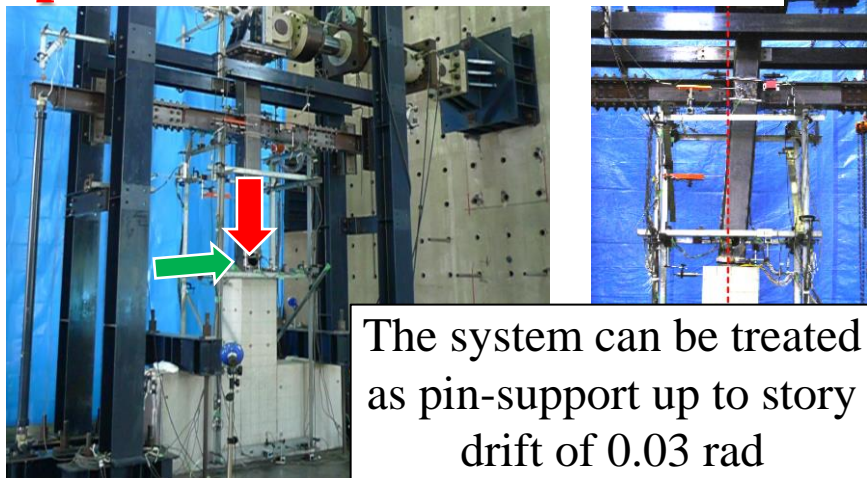
2) Installation of leaning column

Alleviation of damage concentration



Development of new column base system

Understanding mechanical performance of connection



The system can be treated as pin-support up to story drift of 0.03 rad

Loading test on bottom story subassemblies

Manualization

1.3 選した構造形式

2. これまでの設計・施工事例

事例1: 新築建築

事例2: 工場内再生建築

層中間ピン柱脚構法

層中間ピン柱脚構法研究会

建物の用途(実績)
工場、倉庫、事務所、タワニック、保養所等

建物の構造形式
・4層程度の中低層鉄骨構造物
・階高比1.5以下

建物の構造形式
・ラーメン構造
・ラーメン構造+ブレース構造

最下層鉄骨柱の軸力比

長期荷重時	短期荷重時
中柱: 0.20程度 長期の1.3倍	長期の1.3倍
側柱: 0.15程度 長期の1.6倍	長期の1.6倍

RC柱断面寸法
最下層RC柱の幅
→最下層鉄骨柱のせい+内側150mm²⁾

RC柱への作用せん断力
/RC柱のせん断耐力

長期荷重時	短期荷重時
中柱: 0.6程度	0.6程度
側柱: 0.4程度	0.4程度

(1) 規定の適用範囲あり、構法による場合は、別途検討

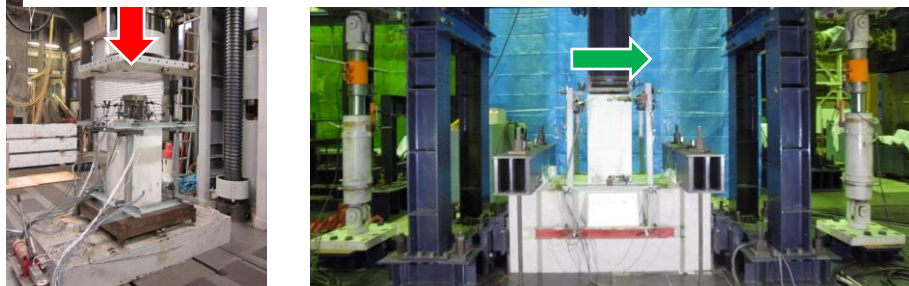
設計上の工夫:

最下層の1階柱については、1F+1.200mmの長さで、短冊型を設けて骨格柱脚構造を採用している。1階ブレース脚柱を省略したに際及び設置に取り付けることにより、1階に必要を許し、必要の必要長さで固定部がとれる。2階の骨格柱脚構造を省略した。内側脚柱は、柱脚部には必要の長さで固定部を設けることにより、骨格柱脚構造は

設計上の工夫:

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Proposition of capacity evaluation formula of connection

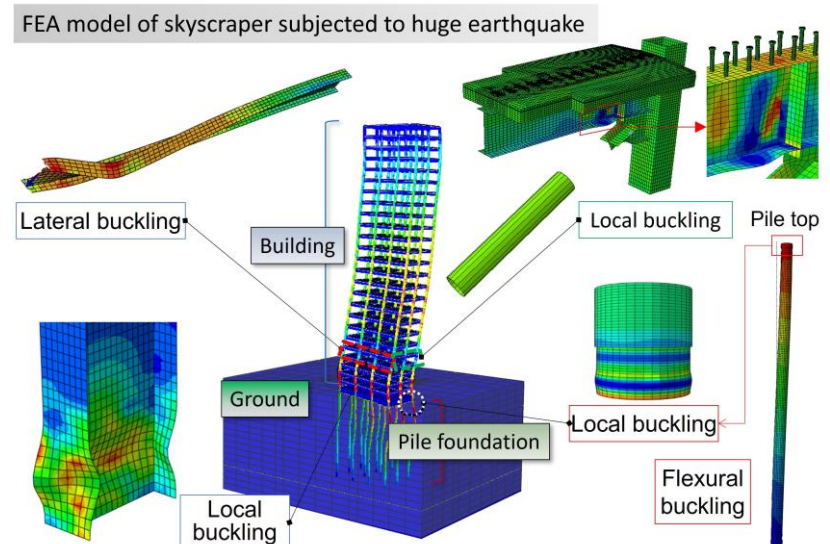


Compression test

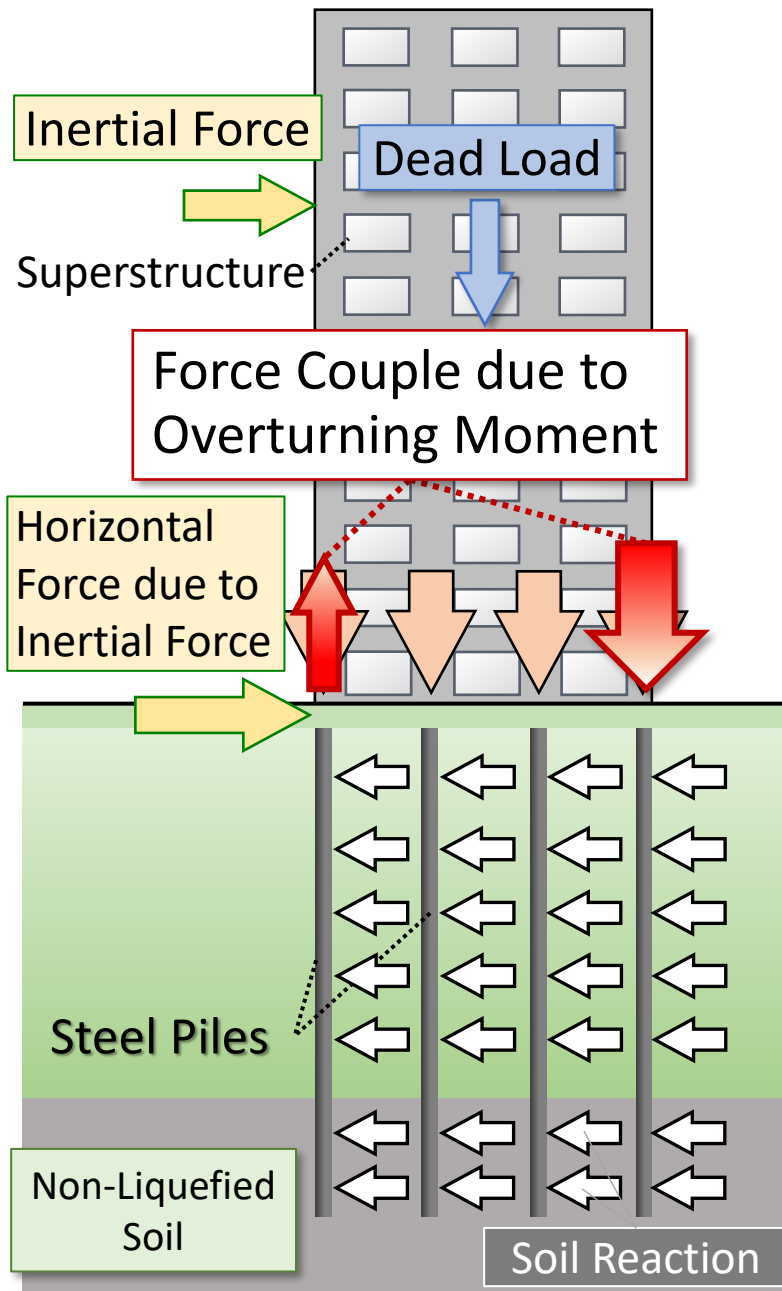
Shear test



Construction of Ultimate State Design Method of Steel Piles and Elucidation of Dynamic Buckling Behavior of Steel Piles in Liquefied Soil



Collapse mechanism of pile



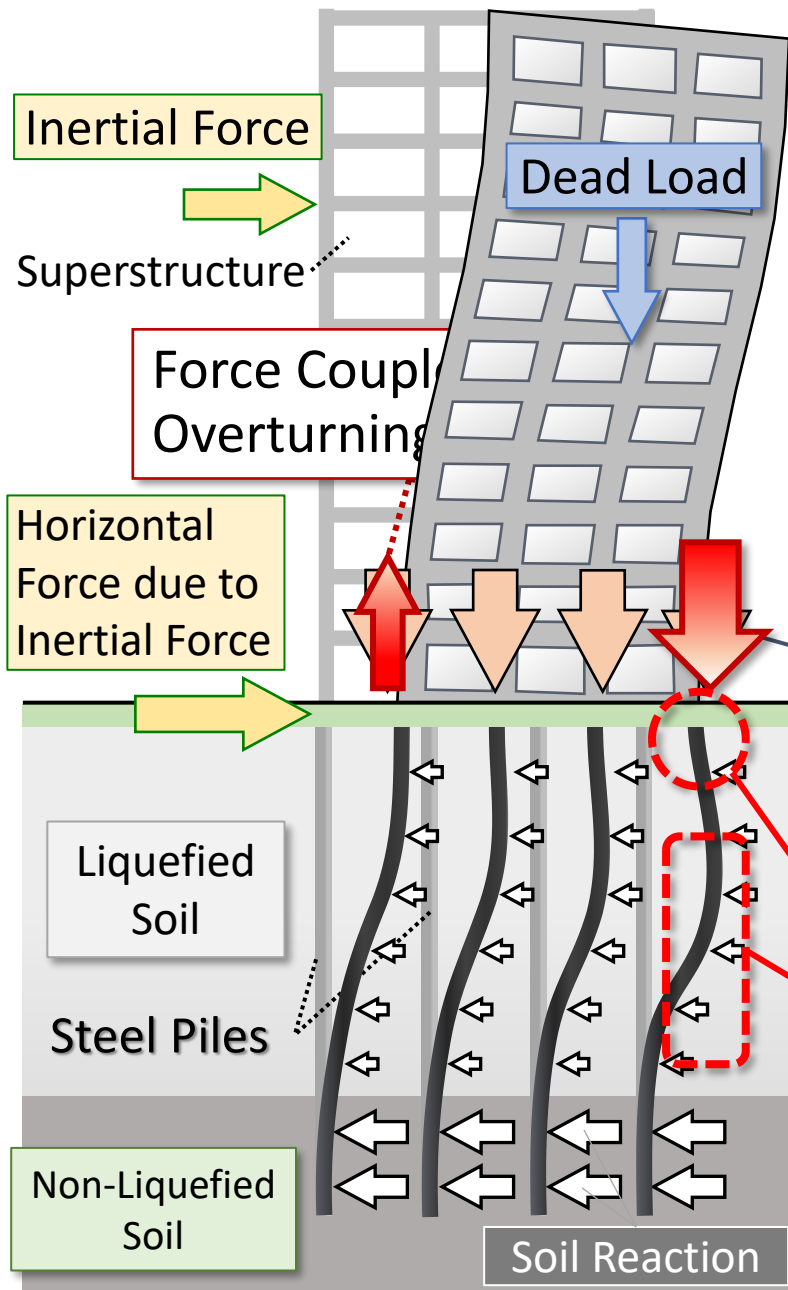
Current Japanese design codes

It is assumed that **steel pile's flexural buckling does not occur** because of soil restriction against piles lateral deformation.

The design codes have **no prescription about the limitation of slenderness** for steel piles.

Reference: Architectural Institute of Japan, Recommendation for Design of Building Foundations, 2001. (in Japanese)

Collapse mechanism of pile

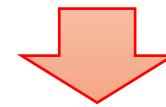


However, when liquefaction occurs during an earthquake,

horizontal stiffness of the ground is reduced drastically.

+

Slender steel piles beneath **high-rise buildings** experience **large axial compression force**.



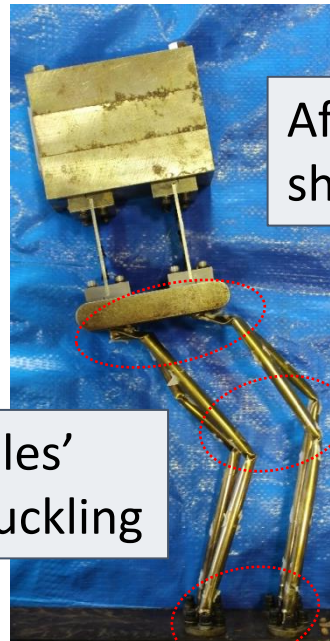
Steel pile's flexural buckling may occur.

Collapse mechanism of pile

◆ Collapse Mechanism of Steel Piles below High-Rise Building in Liquefied Soil

Centrifugal tests of high-rise superstructure, steel piles, and liquefied soil system

under the centrifugal acceleration of 40G



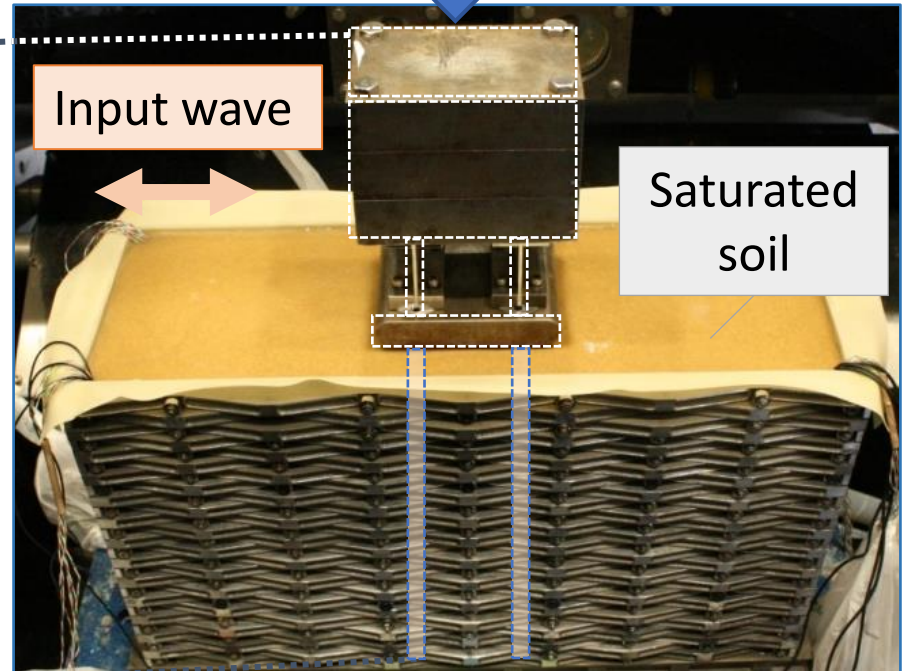
After shaking

Piles' buckling

Ultimate state



Initial state

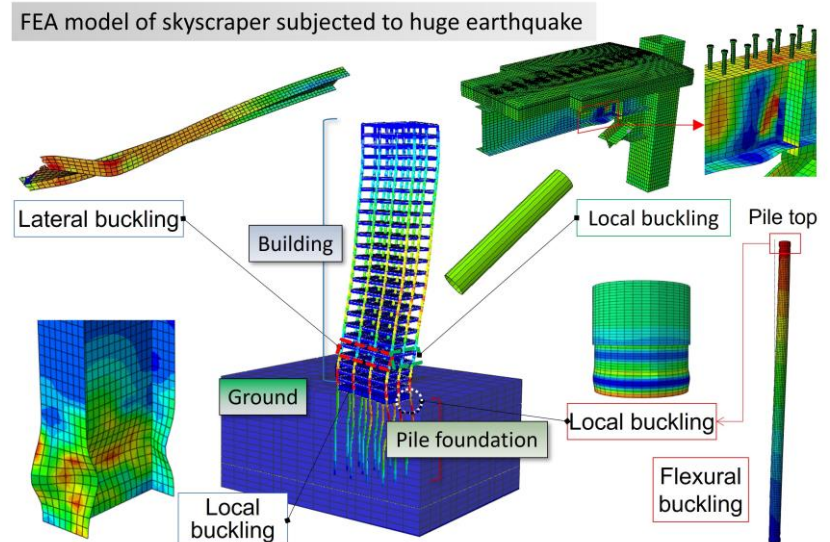


Input wave

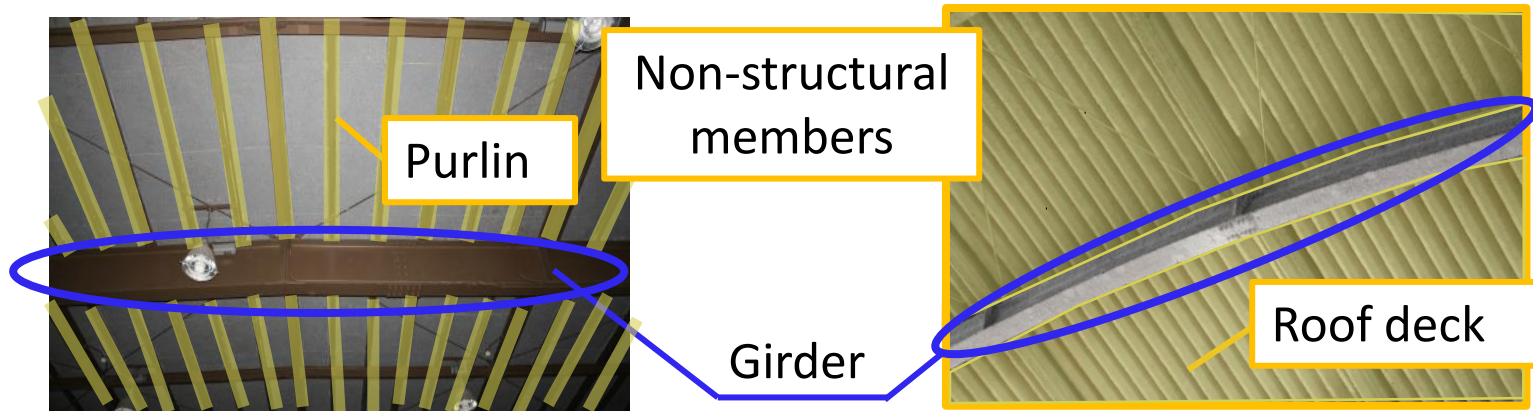
Saturated soil

Specimen for centrifugal test

Invention of Evaluation Method of Lateral Buckling Strength of Large-Span Beams



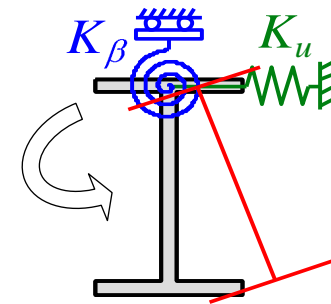
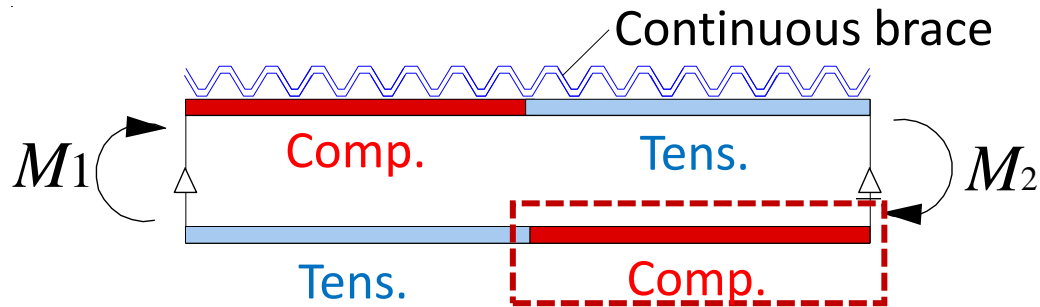
Lateral buckling of I-beam



Non-structural members settle on a top flange (continuous brace)

- Constraint against lateral buckling deformation

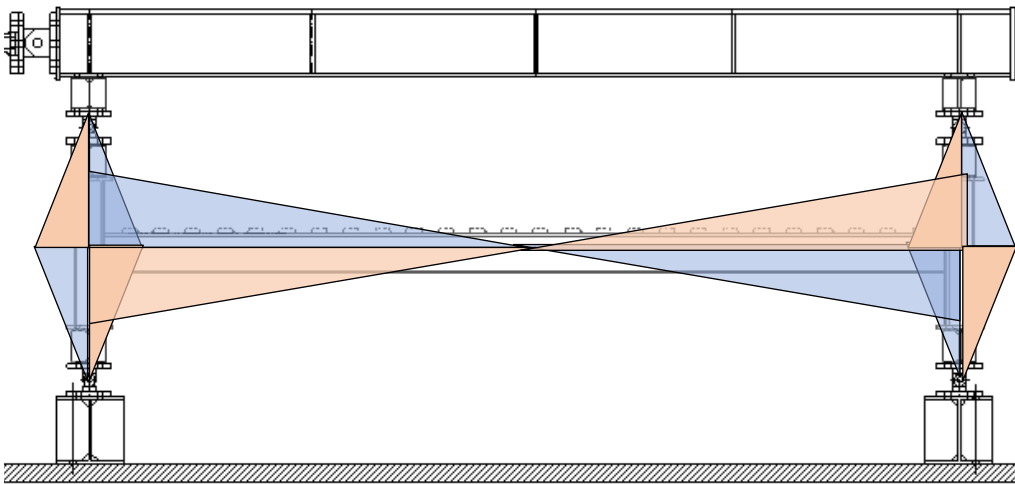
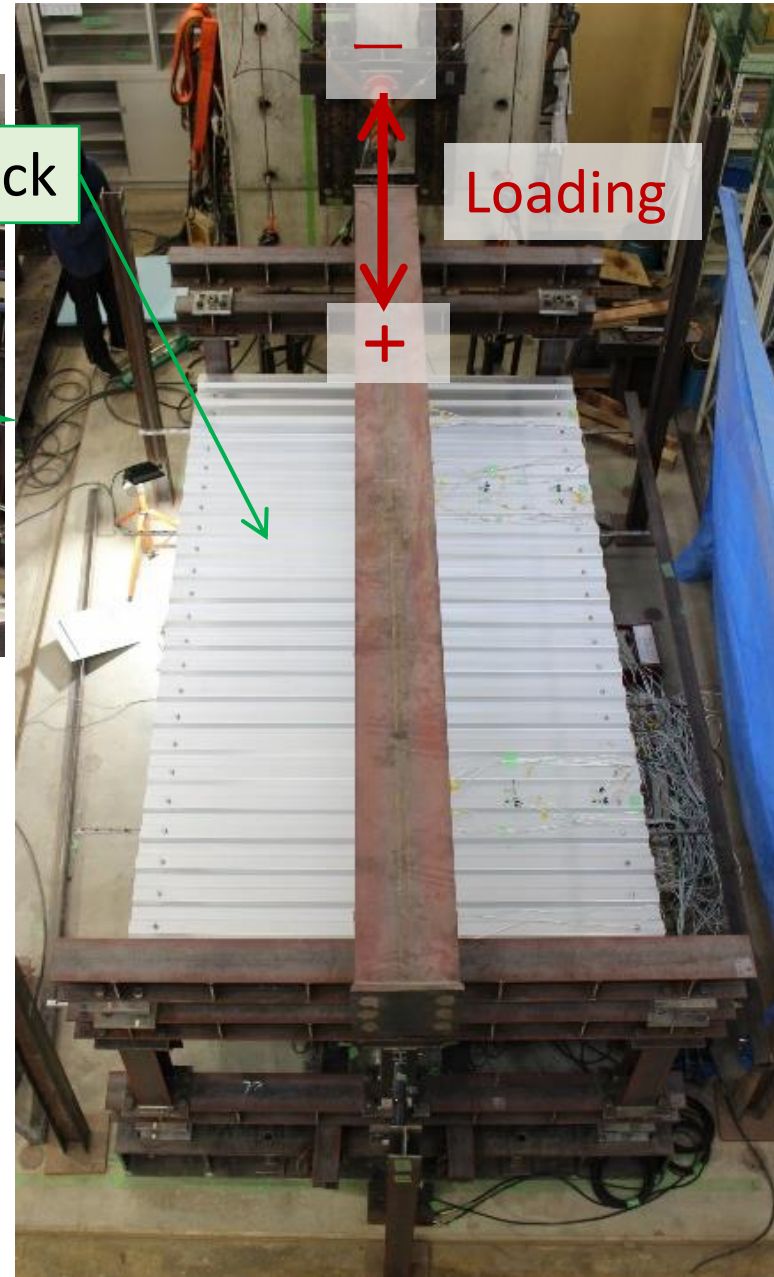
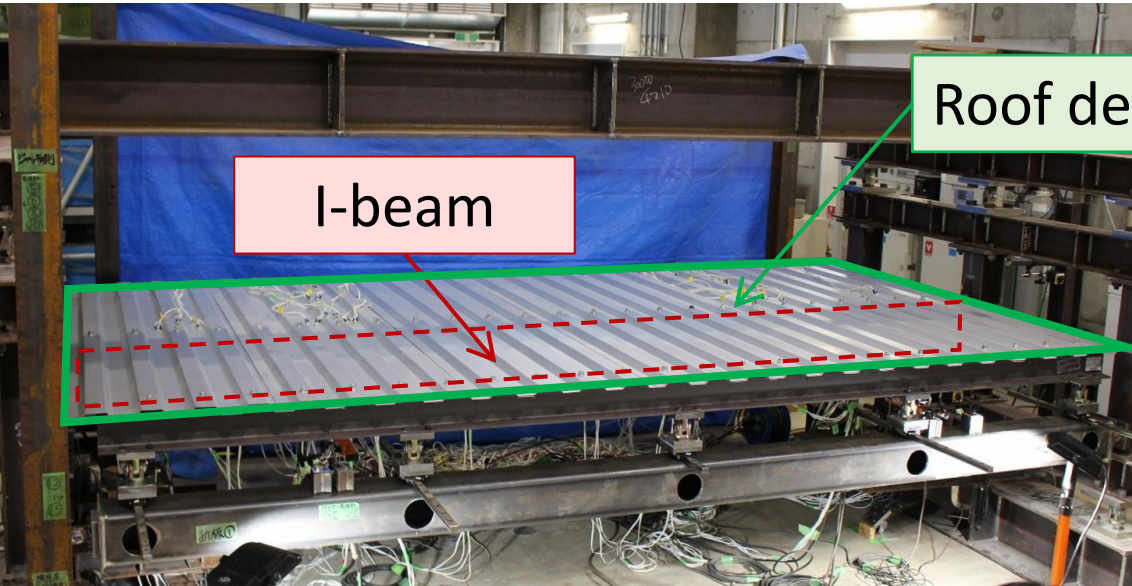
⇒ This effect is ignored in the current design guideline



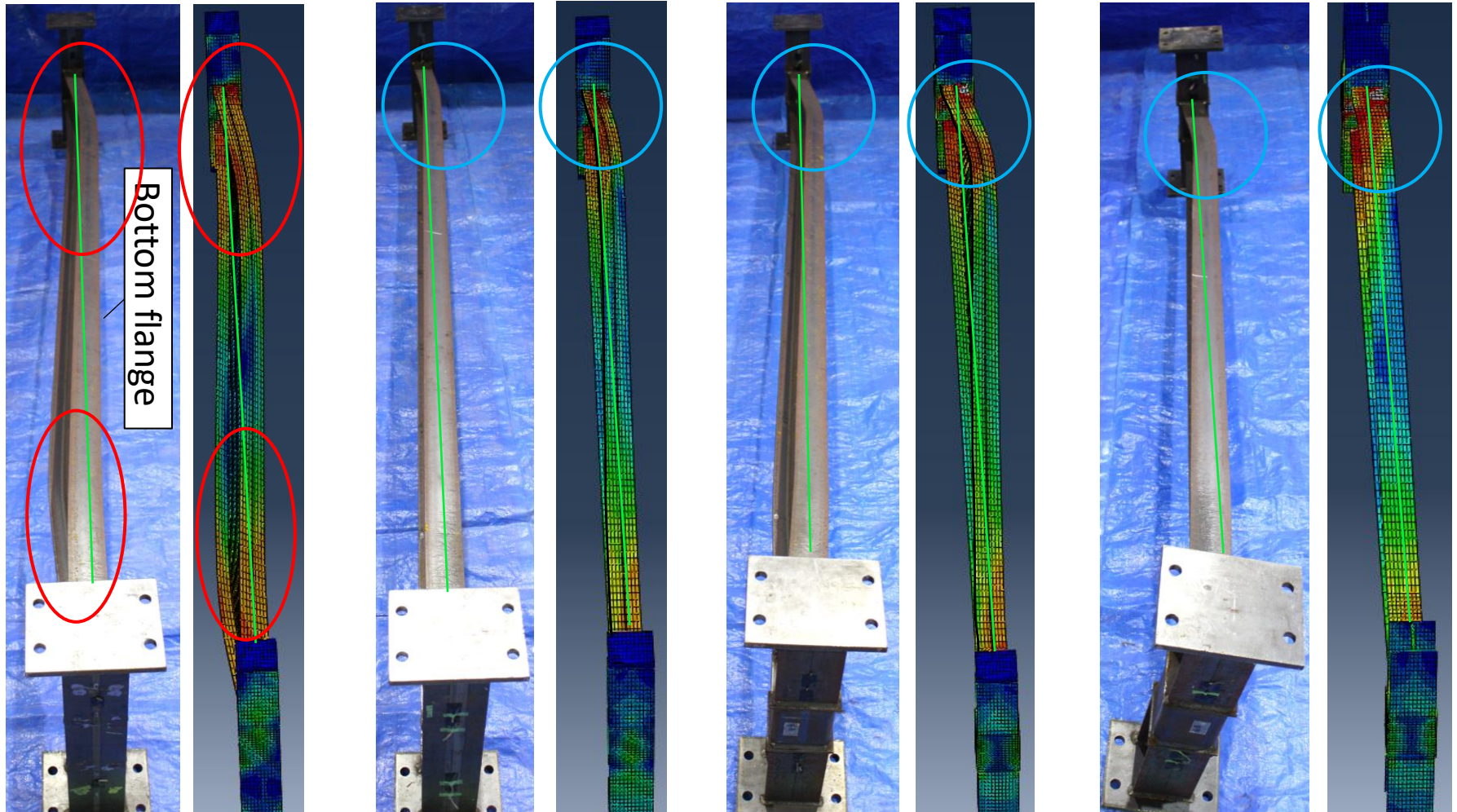
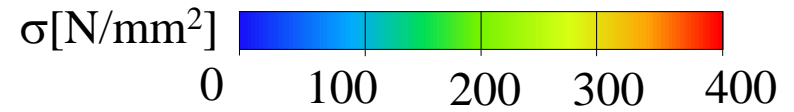
Lateral buckling on bottom flange

→ Bracing on top flange = Horizontal and rotational bracings are necessary

Lateral buckling of I-beam

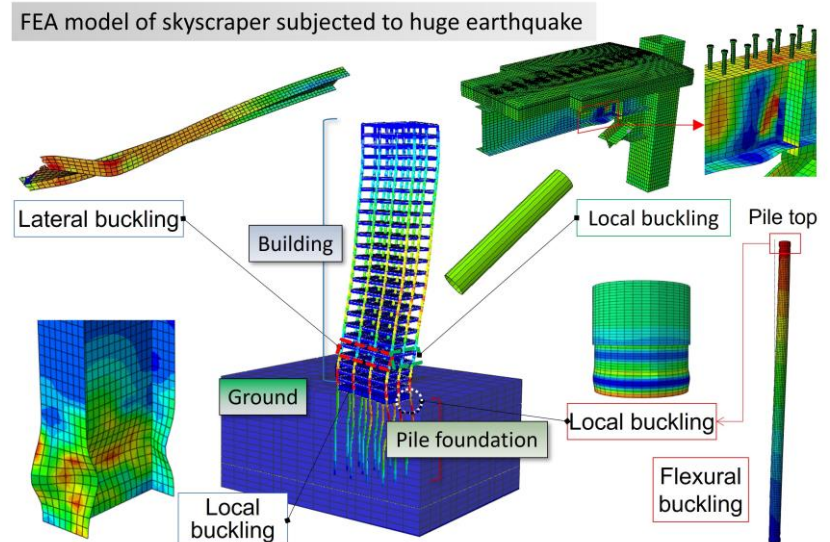


Lateral buckling of I-beam



Buckling behavior is revealed based on experimentation and FEA

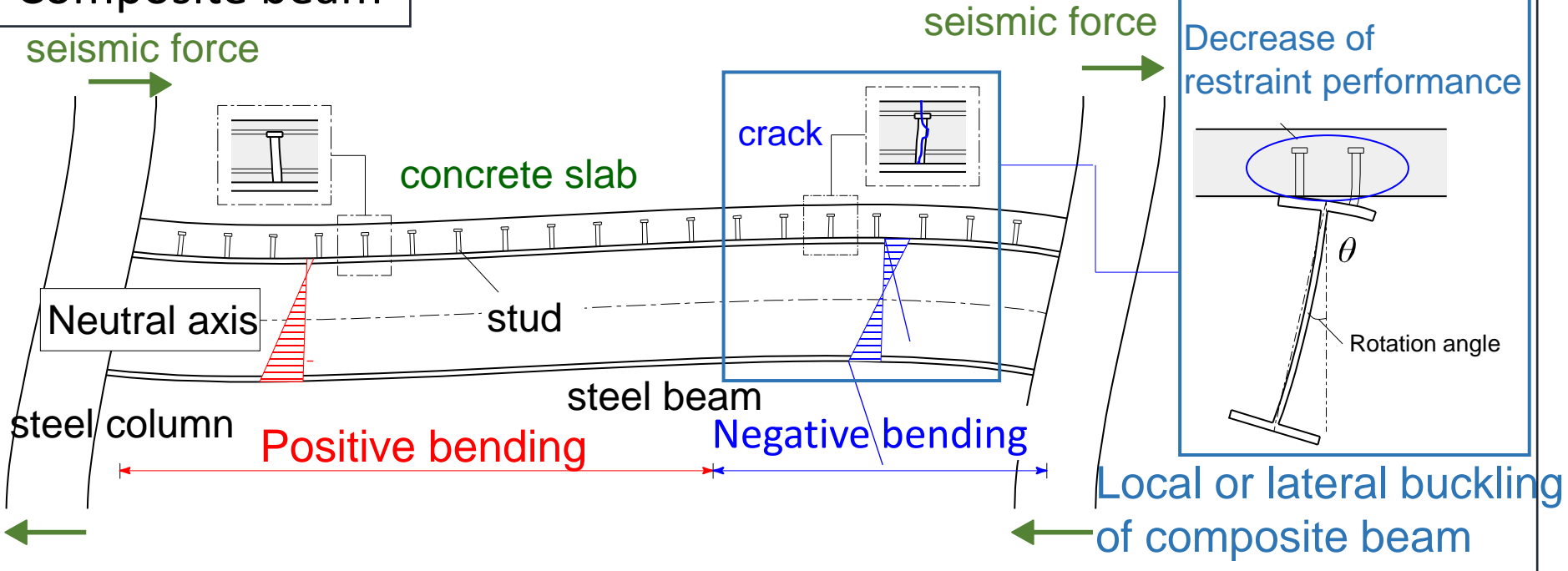
Creation of Seismic Design Method of Buckling Restrained Braced Frame with Concrete Slab



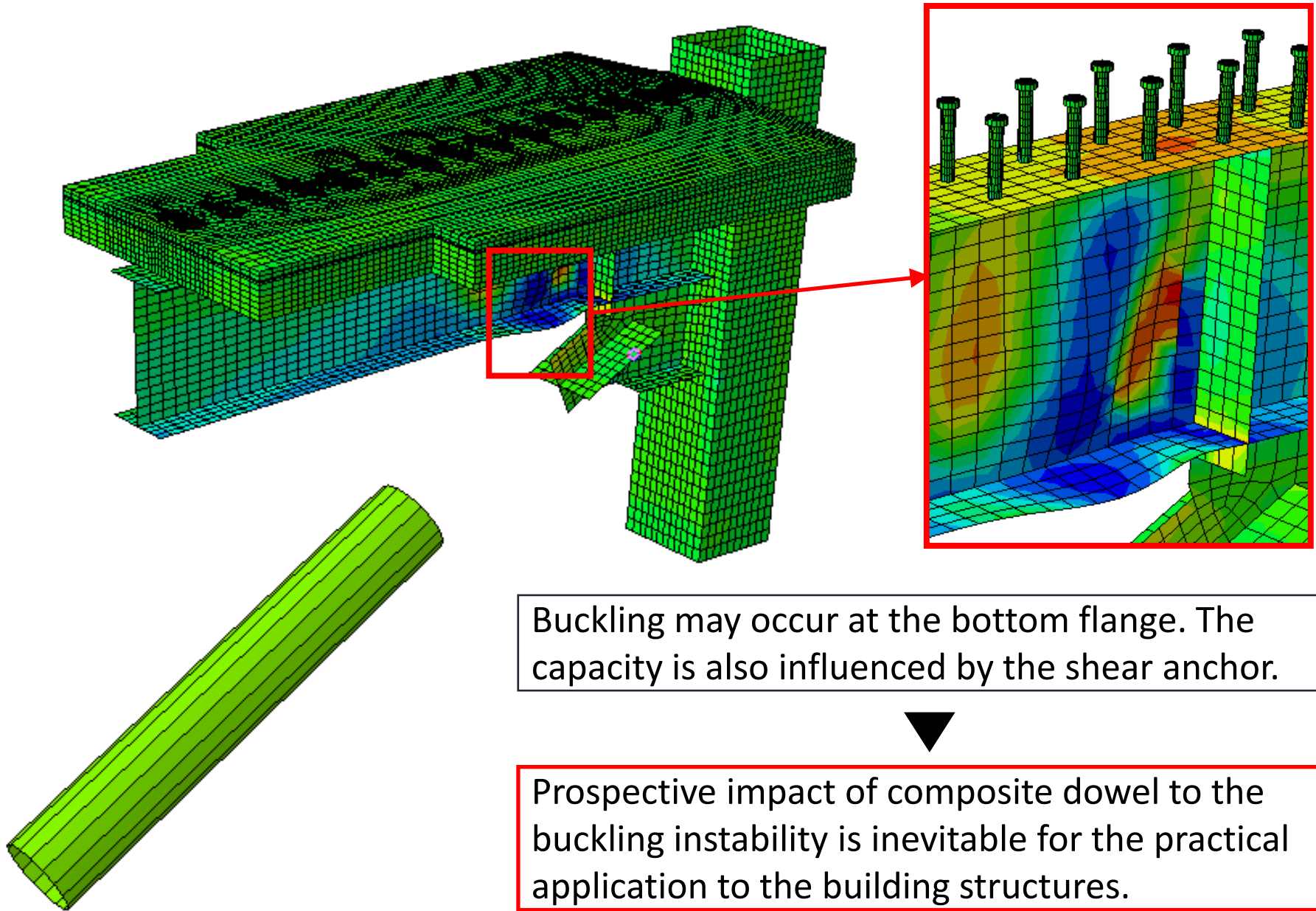
Stress transfer mechanism of composite beam

The neutral axis location varies due to the composite effect during positive bending and negative bending.

Composite beam



Stress transfer mechanism of composite beam



Buckling may occur at the bottom flange. The capacity is also influenced by the shear anchor.

Prospective impact of composite dowel to the buckling instability is inevitable for the practical application to the building structures.